

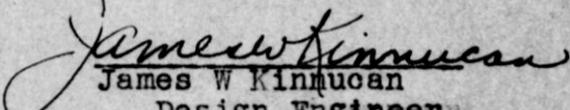
CONTINENTAL AIRCRAFT ENGINE CO.

DETROIT, MICHIGAN

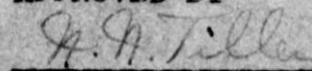
DESIGN REPORT NO. 56
Date April 3, 1934
11 Sheets

CONTINENTAL O-1430-1 ENGINE
LOAD ANALYSIS FOR TWO PROPELLER REDUCTION
GEAR ARRANGEMENTS

PREPARED BY


James W Kinnucan
Design Engineer

APPROVED BY


N. N. Tilley
Chief Engineer

LOAD ANALYSIS FOR TWO PROPELLER REDUCTION GEAR ARRANGEMENTS

Object:- The purpose of this analysis was to determine the loads on the bearings, and surrounding case of the reduction gears, in order that proper consideration might be given to other types of construction than that shown in Continental Report "Design of 1000 H.P. Flat Engine" dated June 22, 1933.

Summary:- The following pages contain an analysis in detail of the original type of construction with a center bearing, called "Construction #1"; and an analysis of a compact type without a center bearing, hereinafter referred to as "Construction #2".

The employment of one diaphragm (Construction "2") to carry, and hence concentrate, the front end loadings into one plane, minimizes the loading on the outer shell of the reduction gear housing.

While the two constructions show differences in rear diaphragm loadings, this is due to the more spread out supports for #1.

The stiffness of the propeller shaft is sufficient to avoid cramping of front end bearing of 1st stage pinion, or throwing of gear teeth out of alignment.

Construction #2 appears somewhat lighter than #1 for same strength and stiffness.

Conclusions: Construction #2 is believed to be best suited for our purpose and is the basis of the present design for the Continental O-1430-1 Engine.

Bearing Loads - Construction #1 with Center bearing

Ratio in first stage = 1.45

Center distance = 6.25 in.

P. D. Pinion = 5.10 in.

P. D. Gear = 7.40 in.

Pitch line velocity = $\frac{5.10 \times 3.1416 \times 3000}{12} = 4000 \text{ ft./min.}$

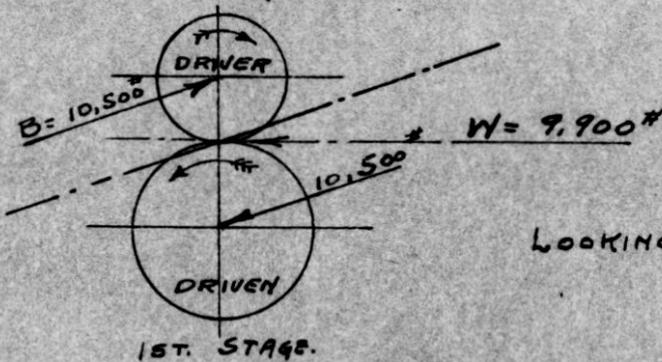
Tangential load = $\frac{1000 \times 33,000}{4000} = 8250 \text{ lb. mean}$

Torque $\frac{\text{Max}}{\text{Mean}}$ for 12 cylinder flat engine = 1.2

8250 x 1.2 = 9,900 lb Max.

P = Bearing pressure for 20° pressure angle (assumed)

$$P = \frac{W}{\cos \alpha} = \frac{9,900}{.93969} = 10,500 \text{ lb.}$$



LOOKING TOWARD PROP. END OF ENGINE

2nd Stage

Ratio = 1.38

Center distance = 6.25 in

P. D. Pinion = 5.250 in. P. D. Gear = 7.250 in.

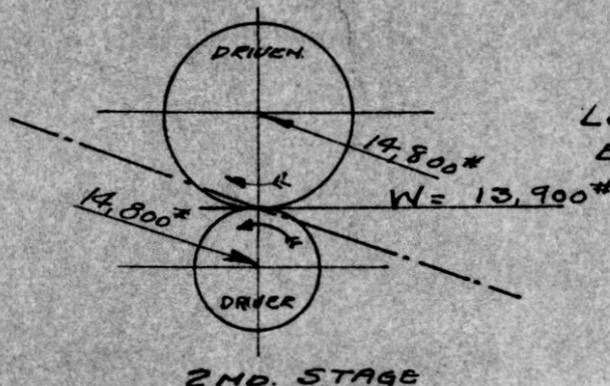
Pitch Line velocity = $\frac{5.250 \times 3.1416 \times 2070}{12} = 2843 \text{ ft./min.}$

Tangential load = $\frac{1000 \times 33000}{2843} = 11,580 \text{ lb. mean}$

11,580 x 1.2 = 13,900 lb. max.

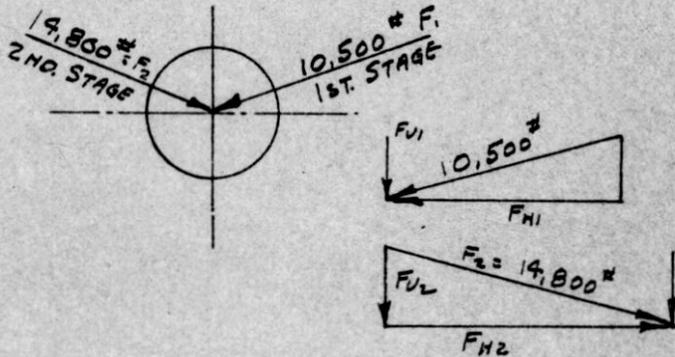
P for bearing pressure $\alpha = 20^\circ$

$$P = \frac{W}{\cos \alpha} = \frac{13,900}{.93969} = 14,800 \text{ lb.}$$



LOOKING TOWARD PROP. END OF ENGINE

Facing forward looking at the end of the jack shaft, we will resolve these forces into their vertical and horizontal components.



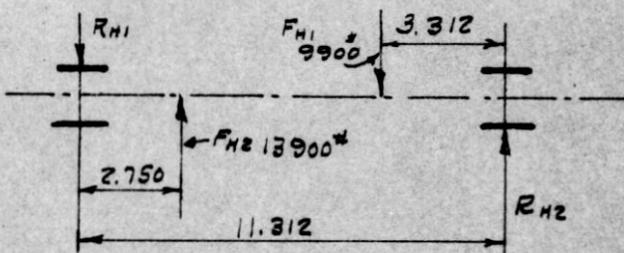
$$F_{V1} = 10,500 \sin 20^\circ = 3600 \text{ lb.}$$

$$F_{H1} = 10,500 \cos 20^\circ = 9900 \text{ lb.}$$

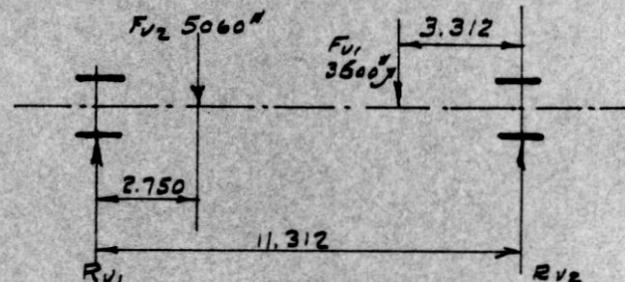
$$F_{V2} = 14,800 \times .342 = 5060 \text{ lb.}$$

$$F_{H2} = 14,800 \times .939 = 13,900 \text{ lb.}$$

We will now pass planes thru the vectors of the forces on the jack shaft.



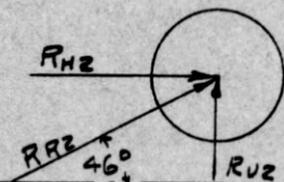
Forces in horizontal plane
 $R_{H1} = 7620 \text{ lb}$ $R_{H2} = 3620 \text{ lb}$



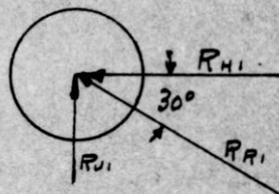
Forces in vertical plane
 $R_{V1} = 4880 \text{ lb}$ $R_{V2} = 3780 \text{ lb}$

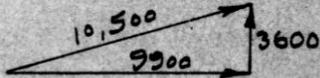
We will now consider the total load on each bearing of the jack shaft.

$$R_{R2} = \sqrt{3780^2 + 3620^2} = 5230 \text{ @ } 46^\circ$$

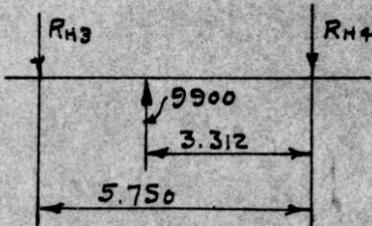


$$R_{R1} = 8850 \text{ @ } 30^\circ$$





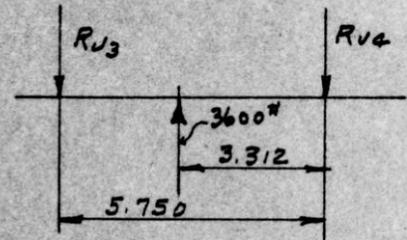
1st. Stage pinion



Forces in horizontal plane

$R_{H3} = 5700$ $R_{H4} = 4200$

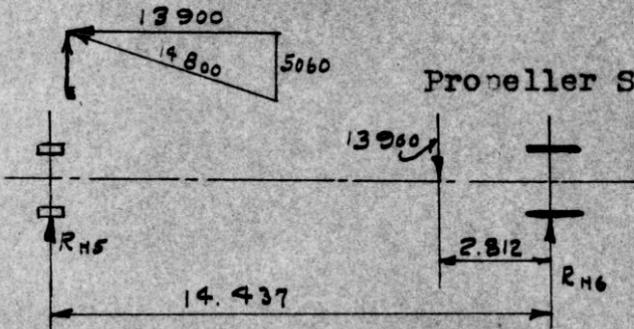
$R_{R4} = 4500 \text{ } @ \text{ } 20^\circ$



Forces in vertical plane

$R_{V3} = 2070$ $R_{V4} = 1530$

$R_{R3} = 6000 \text{ } @ \text{ } 20^\circ$

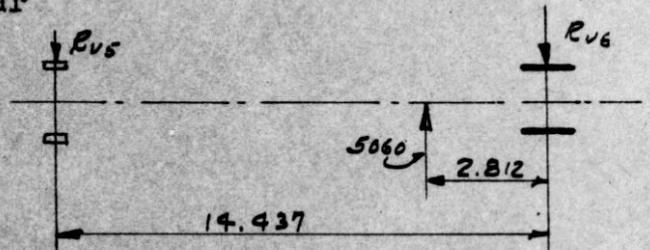


Propeller Shaft Gear

Forces in Horizontal plane

$R_{H5} = 2700$ $R_{H6} = 11200$

$R_{R6} = 12000 \text{ } @ \text{ } 20^\circ$



Forces in vertical plane

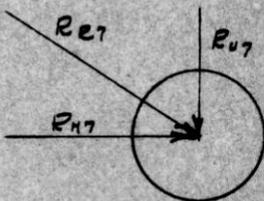
$R_{V5} = 980$ $R_{V6} = 4080$

We will consider the total load on the rear bearing of the propeller shaft.

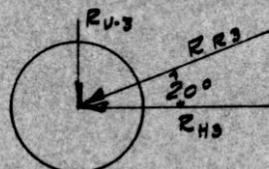
$R_{H6} - R_{H5} = 11200 - 5700 = R_{H7} = 5500 \text{ lb.}$

$R_{V3} + R_{V6} = 4080 + 2070 = R_{V7} = 6150 \text{ lb.}$

$R_{R7} = 8250 \text{ lb. } @ 48^\circ \text{ above horizontal}$

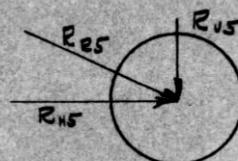


Inside of prop shaft



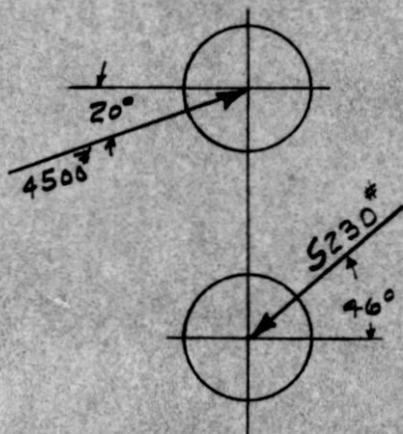
$R_{R3} = 6000 \text{ lb. } @ \text{ } 20^\circ \text{ above horiz}$

Front bearing of prop shaft

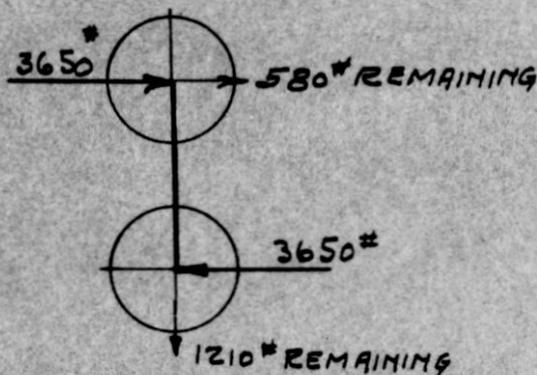


$R_{R5} = 2900 \text{ lb. at } 20^\circ$

By passing a plane thru the diaphragm containing the first stage end bearings,



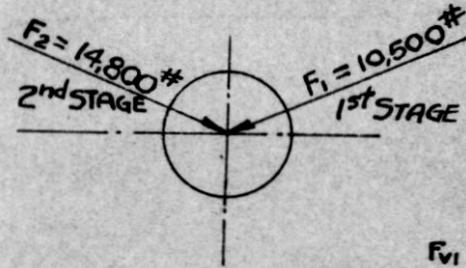
these two forces may be resolved into horizontal and vertical components, leaving a force and a couple acting on the diaphragm.



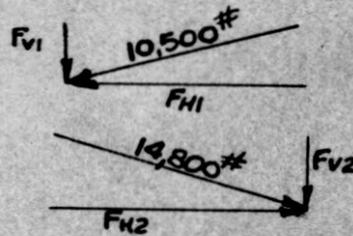
The remaining diaphragms contain only one force as shown on assembly sketch. The reactions of these forces must be taken by the gear case necessitating heavy construction in order to obtain any reasonable degree of rigidity.

Construction #2 -- Without Center Bearing

Facing forward, looking at the end of jack shaft.



We will resolve these forces into their vertical and horizontal components



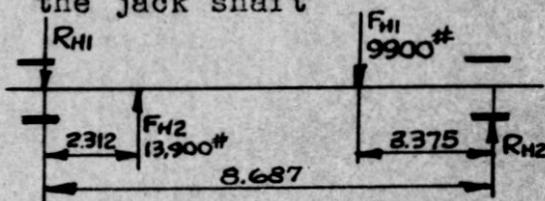
$F_{v1} = 3600 \text{ lb.}$

$F_{h1} = 9900 \text{ lb.}$

$F_{v2} = 5060 \text{ lb.}$

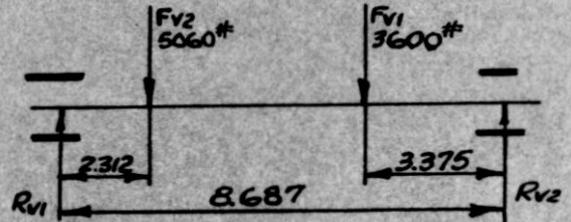
$F_{h2} = 13,900 \text{ lb.}$

We will now pass a plane thru the vectors of the forces on the jack shaft



Forces in horizontal plane

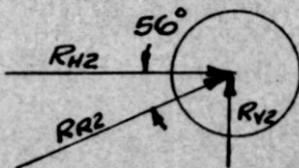
$R_{H1} = 6350 \text{ #}$ $R_{H2} = 2350 \text{ #}$



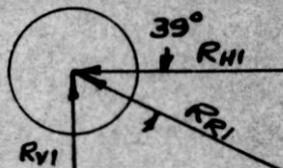
Forces in vertical plane

$R_{v1} = 5120 \text{ #}$ $R_{v2} = 3540 \text{ #}$

We will now consider the total load on each bearing of the jack shaft.

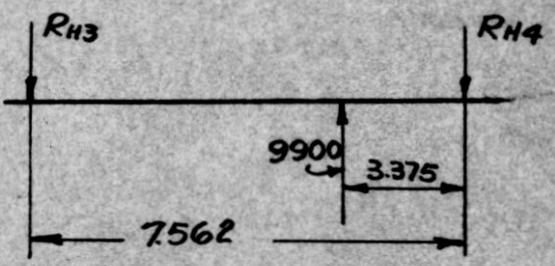


$R_{R2} = 4250 \text{ #} @ 56^\circ$



$R_{R1} = 8160 \text{ #} @ 39^\circ$

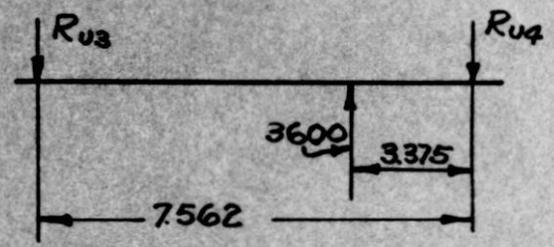
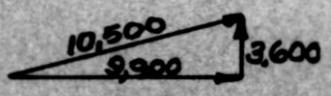
1st Stage Pinion



Forces in horizontal plane

$$R_{H3} = 4400\# \quad R_{H4} = 5500\#$$

$$R_{R4} = 5820\# @ 20^\circ$$

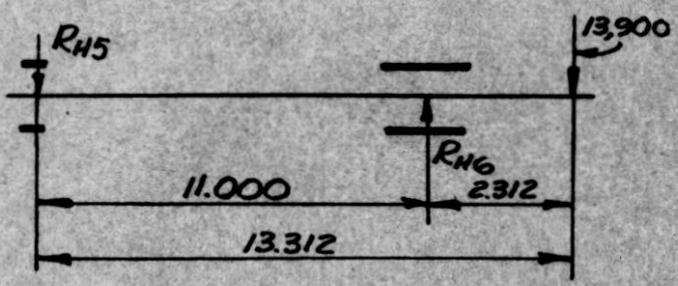


Forces in vertical plane

$$R_{V3} = 1600\# \quad R_{V4} = 2000\#$$

$$R_{R3} = 4680\# @ 20^\circ$$

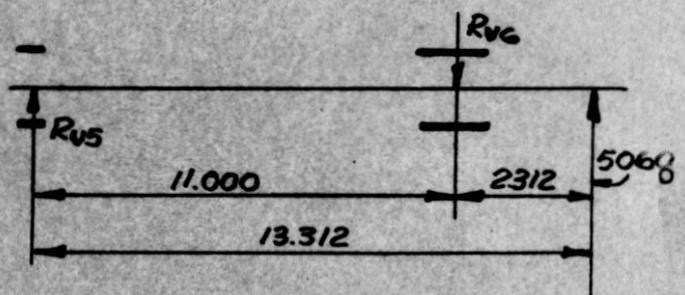
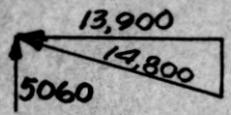
Propeller Shaft Gear



Forces in horizontal plane

$$R_{H5} = 2920\# \quad R_{H6} = 13,900\#$$

$$R_{R5} = 3110\# @ 20^\circ$$



Forces in vertical plane

$$R_{V5} = 1060\# \quad R_{V6} = 5060\#$$

$$R_{R6} = 14,800\# @ 20^\circ$$

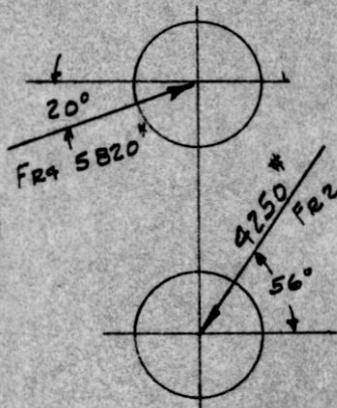
We will now consider the total load on the rear bearing of the propeller shaft.

$$R_{H6} + R_{H3} = R_{H7} = 9,500 \text{ lb.}$$

$$R_{V6} + R_{V3} = R_{V7} = 6,660 \text{ lb.}$$

$$R_{R7} = 11,500 \text{ lb. @ } 35^\circ \text{ above horizontal}$$

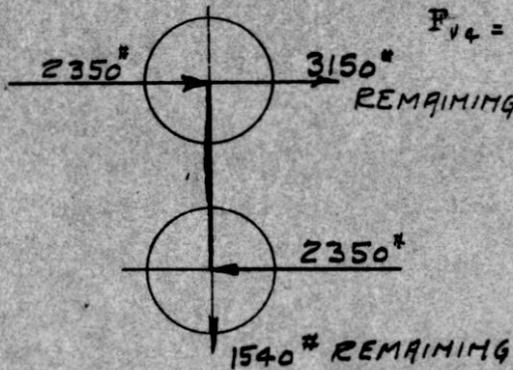
By passing a plane thru the diaphragm containing the first stage end bearing,



these two forces may be resolved into horizontal and vertical components leaving a force and a couple acting on the engine.

$$F_{V2} = 3540 \text{ lb.} \quad F_{H2} = 2350 \text{ lb.}$$

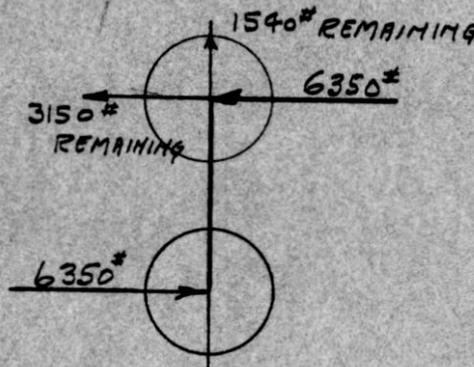
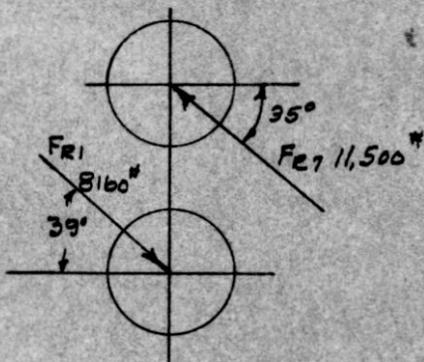
$$F_{V4} = 2000 \text{ lb.} \quad F_{H4} = 5500 \text{ lb.}$$



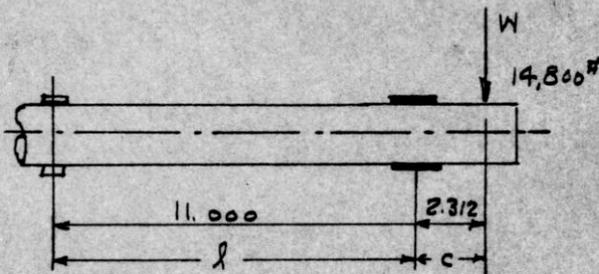
By passing a plane thru the diaphragm containing the second stage forward bearings

$$F_{H7} = 9500 \text{ lb.} \quad F_{V7} = 6660 \text{ lb.}$$

$$F_{H-1} = 6350 \text{ lb.} \quad F_{V-1} = 5120 \text{ lb.}$$



Deflection of Propeller Shaft



I.D. of shaft 3.437

O.D. of shaft 4.125

$$d = \frac{Wc^2}{3EI} (c + l) ; I = \frac{\pi}{64} (D^4 - d^4)$$

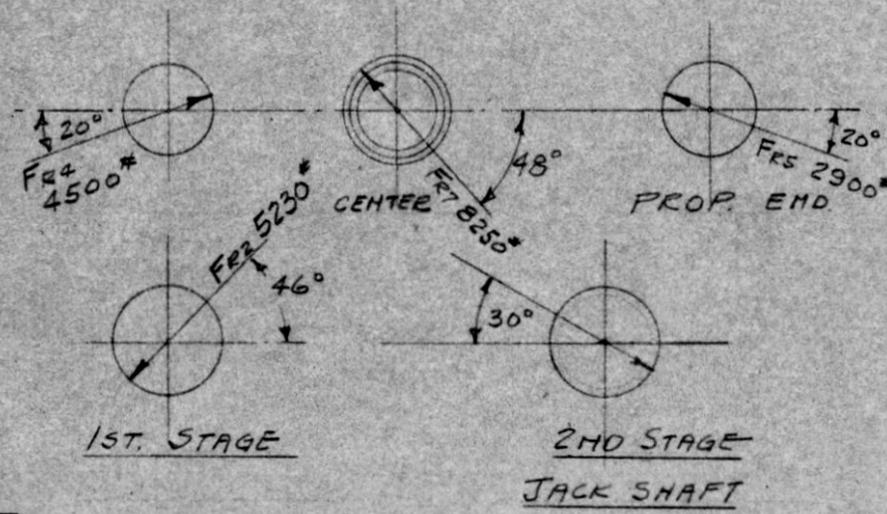
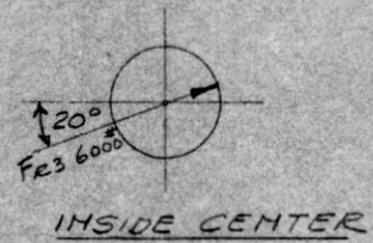
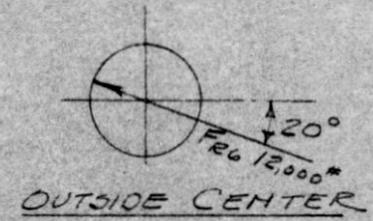
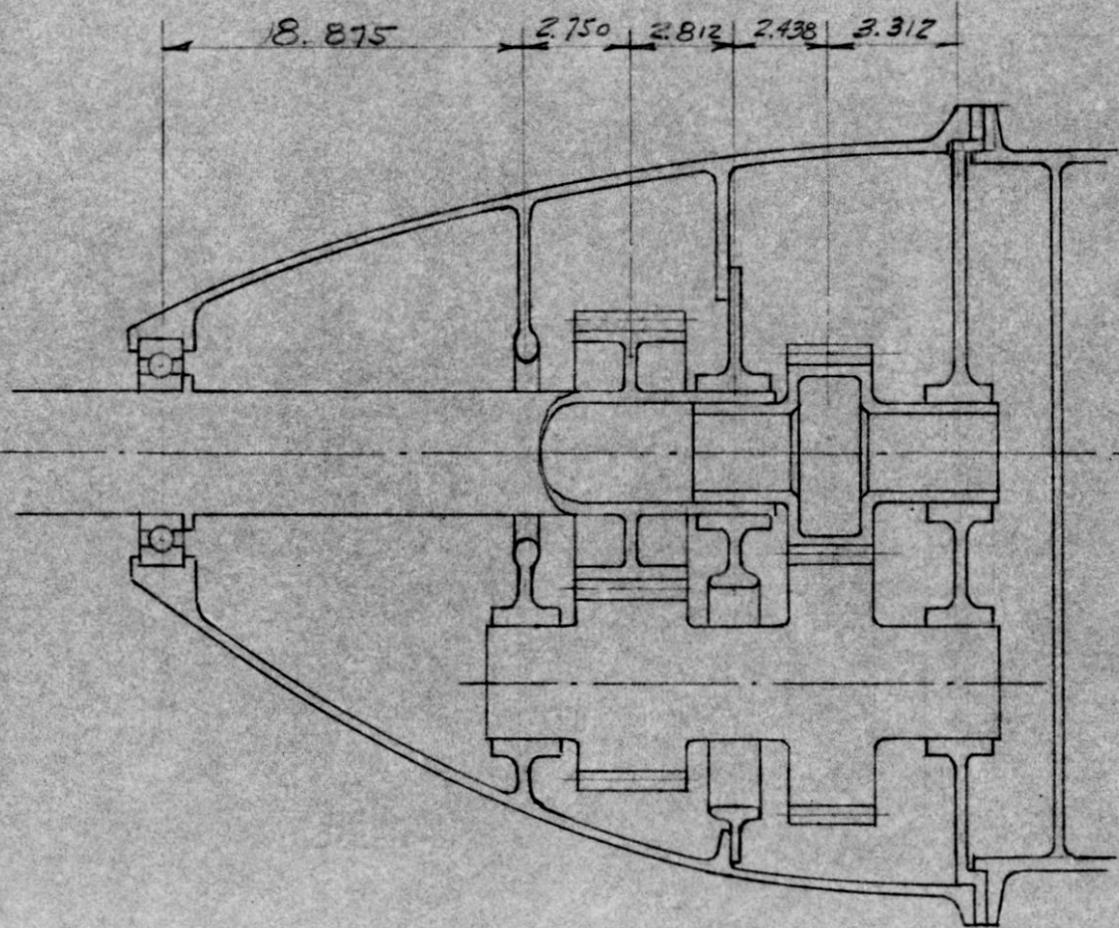
Mchery - Page 343 (Case 8) Max stress $\frac{Wc}{Z}$; $Z = \frac{\pi}{32} \frac{D^4 - d^4}{D}$

$$I = 7.35 \quad c = 2.312 \quad c^2 = 5.34$$

$$d = \frac{14,800 \times 5.34}{3 \times 29,000,000 \times 7.35} = \frac{79,000}{640,000,000} = .000123 \text{ inch}$$

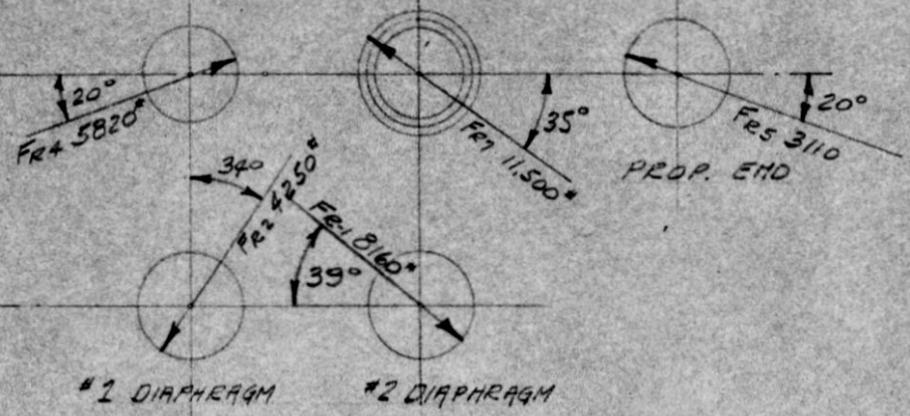
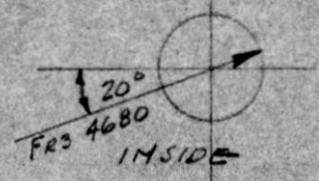
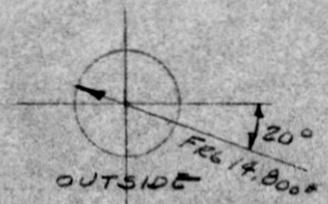
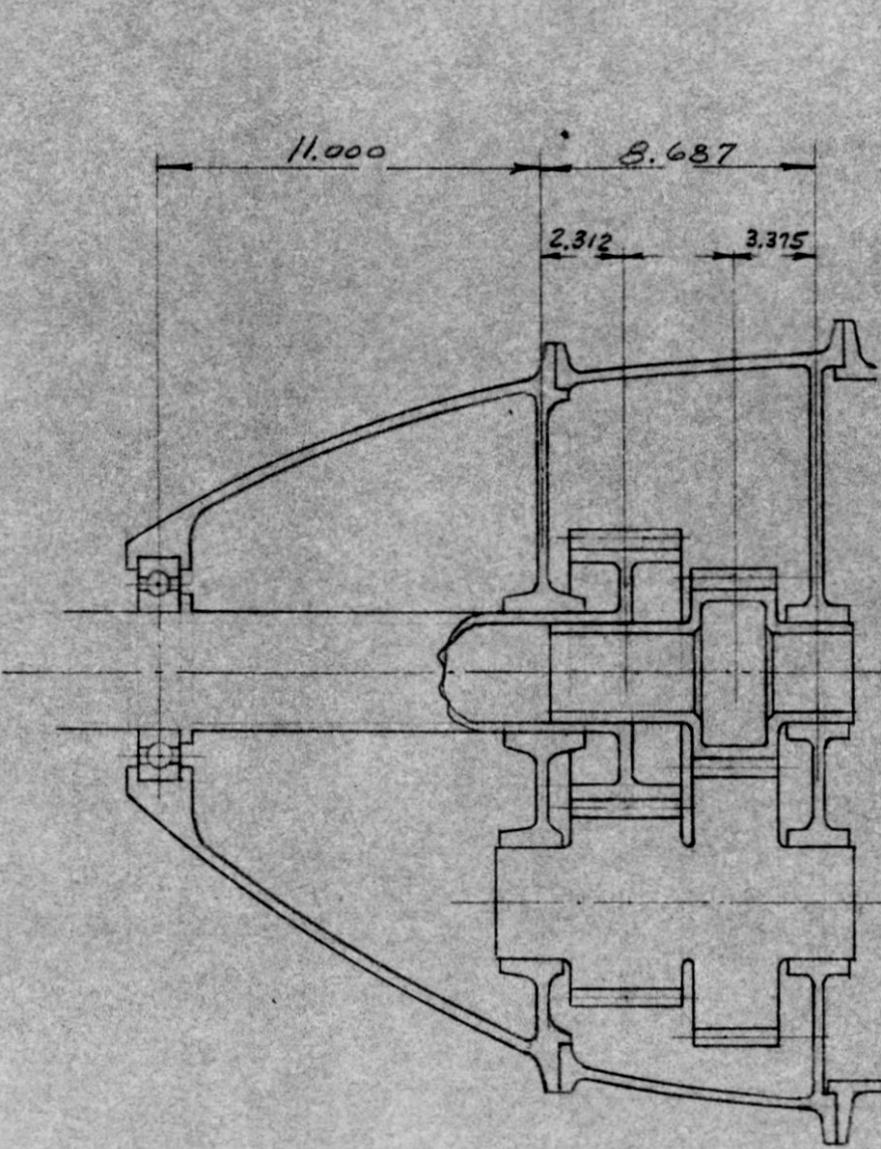
$$\text{Max stress} \quad Z = \frac{I}{R} = \frac{7.35}{2.062} = 3.56$$

$$s = \frac{14,800 \times 2.312}{3.56} = 9,600 \text{ lb. per sq. inch}$$



FORCES ON BEARINGS
1000 H.P. REDUCTION GEARS
CONSTRUCTION No 1
FOR O-1430-1 ENGINE

D.R. 56
 SHEET 10
 APR. 3-34



FORCES ON BEARINGS
1000 H.P. REDUCTION GEARS
CONSTRUCTION NO. 2
FOR O-1430-1 ENGINE

D.R. # 56
 SHEET 11

APR. 3-34